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Tables of Characteristics Slopes for use in the Design of Nozzles for Supersonic Wind Tunnels

By

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SUMMARY

Tables are given which are of use in the calculation of characteristic networks appropriate to two-dimensional nozzles for Mach numbers up to 4.5. The tabulated characteristics slopes enable the co-ordinates of a characteristics intersection each to be evaluated in one operation on a desk calculating machine.

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Fig.

1

1 Introduction

In the design of two-dimensional nozzles for supersonic wind tunnels by the characteristics method the calculations have in many cases been made graphically (for example Harrop and Bright¹). The accuracy can be improved by calculating the characteristics intersections numerically. If the slopes of the characteristics are available the co-ordinates of intersections may each be evaluated in one operation on a desk calculating machine. In designing nozzles for the R.A.E. intermittent wind tunnels the characteristic slopes have been tabulated for characteristic numbers appropriate to Mach numbers up to 4.5 for given characteristic intervals. Even though there should be enough nozzle ordinates available by now to limit further calculations to special cases, and though the characteristics methods is becoming unfashionable, it is felt worth while to make the tables of slopes available generally.

2 List of Symbols

The flow is taken as being from left to right.

- A right up-going characteristic values (in degrees)
- B right down-going characteristic values (in degrees)
- D flow direction
- M Mach number
- m, slope of A characteristics
- -m, slope of B characteristics
- x, y Cartesian co-ordinates
- μ Mach angle
- v Prandtl-Meyer angle

3 Calculation of characteristics slopes

The characteristics method adopted is that of 'points' rather than 'regions'. That is to say values are attributed to the intersections of characteristics of opposite families, rather than to regions enclosed by two pairs of characteristics of opposite families. Consider the intersections of two such pairs as in Fig.1. The 'A' characteristics are taken to be right up-going and the 'B' characteristics right down-going with the flow direction from left to right. It is assumed that the ordinates $(x_1, y_1 \text{ and } x_2, y_2)$ of the intersections of A_1 and B_1 and A_2 and B_2 are known and it is required to find x_3 and y_3 . Then if the mean slopes of the characteristics approaching $x_3 y_3$ are m_1 and $-m_2$ we have

$$x_{3} = \frac{y_{2} - y_{1} + m_{1}x_{1} + m_{2}x_{2}}{m_{1} + m_{2}}$$
(1)

$$y_{3} = \frac{x_{2} - x_{1} + \frac{y_{1}}{m_{1}} + \frac{y_{2}}{m_{2}}}{\frac{1}{m_{1}} + \frac{1}{m_{2}}}.$$
 (2)

Thus if the values m_1 , m_2 , $m_1 + m_2$ and $\frac{1}{m_1}$, $\frac{1}{m_2}$, $\frac{1}{m_1} + \frac{1}{m_2}$ are tabulated the co-ordinates $x_3 y_3$ can be obtained immediately with the use of a desk calculating machine.

The slopes m_1 and m_2 are given by

$$m_1 = \tan(\mu_1 + D_1)$$
 (3)

$$m_2 = \tan \left(\mu_2 - D_2\right) \tag{4}$$

where μ_1 , D_1 and μ_2 , D_2 are the mean values of the Mach angle and flow direction respectively along the lines x_1 , y_1 : x_3 , y_3 , and x_2 , y_2 : x_3 , y_3 .

The values of μ and D are derived from the characteristics numbers in the usual way, i.e.

$$v_1 = A_1 + \frac{1}{2}(B_1 + B_2)$$

where for $\gamma = 1.4$ the Prandtl-Meyer angle^{*}

$$\nu = \mu + \sqrt{6} \operatorname{arc cot} (\sqrt{6} \tan \mu) - \frac{1}{2}\pi$$

and

$$D_{1} = \frac{1}{2}(B_{1} + B_{2}) - A_{1}$$

$$\nu_{2} = B_{2} + \frac{1}{2}(A_{1} + A_{2})$$

$$D_{2} = B_{2} - \frac{1}{2}(A_{1} + A_{2})$$

The values of
$$\nu$$
 were taken from the tables of Herbert and Older²
and the tangents of the angles from Hilne-Thomson and Comrie³.

The errors in the tables should not exceed 2 units in the last decimal place quoted.

-* The subtraction of ν from 1000 in order to obtain the so-called pressure number appears to be a fruitless operation.

4 Description of Tables

The tables are set out with given values of A along rows and given values of B down columns. Each block of six numbers gives values of the two slopes and their sum and similarly for the reciprocals. The values refer to the slopes of characteristics approaching a given point A, B, with the appropriate interval. As A, B increase the value of the interval is increased progressively. The intervals in degrees are

Table I	0.2			М	<	1.22
Table II	0.4	1.2	<	M	<	1.43
Table III	0.8	1.43	<	М	<	1.81
Tables IV and V	1.6	1.81	<	М	<	4.53

M being the Mach number appropriate to the characteristic numbers on the centre-line of a nozzle.

The selection of the values of A in Table I perhaps needs some explanation. It will be noted that the values have a minimum in the middle of the range. The minimum arises because the values are designed to be used in the throat region of a nozzle, where constant Mach number lines are convex downstream (see e.g. Fig.1 of Ref.1). A right down-going characteristic is thus tangential to some constant Mach number line. The right up-going characteristic through the point of tangency will therefore have a minimum value.

REFERENCES

<u>No</u> .	Author	Title, etc.									
1	R. Harrop and P.I. Bright	Design and testing of supersonic nozzles Part I R c. M 2712 October, 1948.									
2	P.J. Herbert and	Tables for use in the investigation of supersonic									

S.J. Older fields of flow by the method of characteristics R.A.E. Tech. Note No. CW1 November, 1946. ARU 10.261
J.M. Milne-Thomson and L.J. Comrie Macmillan 1948.

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Slopes refer to characteristics approaching point (A, B)

Table I - Characteristic Slopes Interval 0.20

Key

AR	0.9		1.1			1	1.3			1.5	· · · · · · · · · · · · · · · · · · ·	1	1.7		· · · · · · · · · · · · · · · · · · ·	1 0			0.4		
2.1	1.5527	1.7056	3.2583	1-5255	1.6481	3.1736	1.5005	1_5953	3.0958	4 1.778	4 51.66	3 024	4 1560	4 5047			1.7			2.1	
	0.6441	0.5863	1.2304	0.6556	0.6067	1.2623	0.6664	0.6268	1.2932	0.6767	0.6466	1.3233	0.6864	0.6661	1.3525	0.6956	0.6853	2.8967	1.4197 0.7044	1.4197 0.7044	2.8394
1.9	1.6075	1.7401 0.5747	3.3476 1.1968	1.5767 0.6342	1.6786 0.5957	3.2553 1.2299	1.5489 0.6456	1.6225 0.6163	3.1714 1.2619	1.5236 0.6564	1.5709 0.6366	3.0945 1.2930	1.5002	1.5232 0.6565	3.0234 1.3230	1.4789 0.6762	1.4789	2.9578	1.4592	1.4375	2.8967
1.7	1.6676 0.5997	1.7783 0.5623	3.4459 1.1620	1.6328 0.6125	1.7123 0.5841	3.3451 1.1966	1.6013 0.6245	1.6522 0.6052	3.2535 1.2297	1.5729 0.6358	1.5974 0.6260	3.1703 1.2618	1.5470	1.5470 0.6464	3.0940 1.2928	1.5232	1.5002	3.0234	1.5013	1.4569	2.9582
1.5	1.7342 0.5766	1.8212 0.5491	3.5554 1.1257	1.694.3 0.5902	1.7496 0.5716	3.4439 1.1618	1.6586	1.6851 0.5935	3.3437 1.1964	1.6265 0.6148	1.6265	3.2530 1.2296	1.5974	1.5729	3.1703	1.5709	1.5236	3.0945	1.5466	1.4778	3.0244
1.3	1.8085 0.5529	1.8697 0.5349	3.6782 1.0878	1.7625 0.5674	1.7915 0.5582	3.5540 1.1256	1.7216	1.7216	3.4432 1.1616	1.6851	1.6586	3.3437	1.6522	1.6013	3.2535	1.6225	1.5489	3.1714	1.5953	1.5005	3.0958
1.1	1.8926 0.5 <i>2</i> 83	1.9250 0.5195	3.8176 1.0478	1.8387 0.5439	1.8387	3.6774 1.0878	1.7915	1.7625	3.5540 1.1256	1.7496 0.5716	1.6943	3.4439	1.7123	1.6328	3.3451	1.6786	1.5767	3.2553	1.6481	1.5255	3.1736
0.9	1.9890 0.5027	1.9890 0.5027	3.9780 1.0054	1.9250	1.8926 0.5283	3.8176 1.0478	1.8697	1.8085	3.6782 1.0877	1.8212 0.5491	1.7342	3.5554	1.7783	1.6676	3.4459	1.7401 0.5747	1.6075	3.3476	1.7056	1.5527	3.2583
0.7	2.1012 0.4759	2.0640 0.4845	4.1652 0.9604	2.0242 0.4940	1.9550 0.5115	3.9792 1.0055	1.9584 0.5106	1.8611	3.8195 1.0479	1.9015 0.5259	1.7791	3.6806	1.8518	1.7065	3.5583 1.1260	1.8078	1.6415	3.4493	1.7685	1.5827	3.3512
0.5	2.2355 0.4473	2.1543 0.4642	4 . 3898 0.9115	2.1396 0.4674	2.0278 0.4932	4.1674 0.9606	2.0603 0.4854	1.9218 0.5204	3.9821 1.0058	1.9926 0.5018	1.8303	3.8229 1.0482	1.9342	1.7504	3.6846 1.0883	1.8831	1.6795	3.5626	1.8380 0.5001	1.6160	3.4540
0.3	2•3988 0•4170	2.2641 0.4417	4.6629 0.8587	2.2781 0.4389	2.1155 0.47 <i>2</i> 7	4.3936 0.9116	2.1792 0.4588	1.9925 0.5018	4-1717 0-9606	2.0974 0.4767	1.8895	3.9869	2.0278	1.8003	3.8281 1.0486	1.9677	1.7223	3.6900	1.9153	1.6532	3,5685
0.1	2.6092 0.3833	2.3298 0.4292	4.9390 0.8125	2.4468 0.4087	2.1662 0.4616	4.6130 0.8703	2,3220 0,4307	2.0332 0.4918	4.3552 0.9225	2.2199 0.4504	1.9226	4.1425	2.1357 0.4682	1.8280	3.96 <i>3</i> 7 1.0152	2.0640	1.7461 0.57 <i>2</i> 7	3.8101	2.0022	1.6735	3.6757
0.1	2.6092 0.3833	2,2641 0,4417	4.8733 0.8250	2.4468 0.4087	2.1155 0.4727	4.5623 0.8814	2.3220 0.4317	1.9925 0.5018	4 • 3145 0 • 9325	2.2199 0.4504	1.8895	4.1094 0.9797	2.1357 0.4682	1.8003	3.9360 1.0236	2.0640	1.7223	3.7863	2.0022	1.6532	3.6554
0.3	2 . 3988 0.4170	2.1543 0.4642	4•5531 0.8812	2.2781 0.4389	2.0278 0.4932	4.3059 0.9321	2.1792 0.4588	1.9218 0.5204	4.1010 0.9792	2.0974 0.4767	1.8303 0.5464	3.9277 1.0231	2.0278 0.4932	1.7504	3.7782 1.0645	1.9677	1.6795	3.6472	1.9153 0.5221	1.6160	3.5313
0.5	2.2355 0.4473	2.0640 0.4845	4•2995 0•9318	2 .1 396 0 . 4674	1.9550 0.5115	4.0946 0.9789	2.0603 0.4854	1.8611 0.5373	3.9214 1.0227	1.9926 0.5018	1.7791	3.7717 1.0639	1.9342 0.5170	1.7065 0.5860	3.6407	1.8831	1.6415	3.5246	1.8380	1.5827	3.4207
0.7	2.1012 0.4759	1.9890 0.5027	4.0902 0.9786	2.0242 0.4940	1.8926 0.5283	3.9168 1.0223	1.9584 0.5106	1.8085	3.7669	1.9015 0.5259	1.7342 0.5766	3.6357	1.8518	1.6676	3.5194 1.1397	1.8078	1.6075	3.4153	1.7685	1.5527	3.3212
0.9				1.9250 0.5 1 95	1,8387 0,5439	3.7637 1.0634	1.8697 0.5348	1.7624 0.5674	3.6321	1.8212 0.5491	1.6943	3.5155 1.1393	1.7783	1.6328	3.4111	1.7401	1.5767	3.3168	1.7056	1.5255 0.6556	3.2311
1.1							1.7915	1.7216	3.5131	1.7496	1.6586	3.4082 1.1745	1.7123	1.6013	3.3136 1.2086	1.6786	1.5489	3.2275	1.6481	1.5005	3.1486
1.3										1.6851	1.6265	3.3116	1.6522	1,5729 0,6358	3.2251	1.6225	1.5236	3.14.61	1.5953	1.4778	3.0731
1.5							}				,		1.5974 0.6260	1.5470 0.6.6.	3.1444	1.5709	1.5002	3.0711	1.5466	1.4569	3.0035
1.7														up up	· • - (- 4	1.5232	1.4789	3.0021	1,5013	1.4375	2.9388
1.9					ľ			,									APOLOC	1.5741	1.4592 0.6853	1.4197 0.70	2.8789
┝━━┅━━━━┫┉	••d.,			1		<u></u>	<u> </u>											1		~ • / • • • •	

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Flow from left to right A Right up-going characteristic (in degrees) B Right down-going characteristic (in degrees)

7	^m 1	^m 2	^m 1 + ^m 2
	1/11_1	1/m ₂	$1/m_1 + 1/m_2$

TABLE	IA

Characteristic Slopes	Interval 0.4°				
Slopes refer to characteristics approaching point (A, B) Flow from left to right A Right up-going characteristic (in degrees) B Right down-going characteristics (in degrees)	;	Кеу	^m 1 1/m ₁	^m 2 1/m ₂	$m_1 + m_2$ 1/m_1 + 1/m_2

B		1.1			1.5	-		1.9		2.5			
3.7	1.2295 0.8134	1.4868 0.6726	2.7163 1.4860	1.2061 0.8291	1.4144 0.7070	2.6205 1.5361			Ĩ				
3.3	1.2927 0.7735	1.5211 0.6575	2.8138 1.4310	1.2651 0.7905	1.4429 0.6930	2.7080 1.4835	1.2410 0.8058	1.3733 0.7282	2.614 <i>3</i> 1.5340	1.2149 0.8231	1.2814 0.7804	2.4963 1.6035	
2.9	1.3639 0.7332	1.5608 0.6407	2.92,7 1.3739	1.3308 0.7514	1.4757 0.6777	2.8065 1.4291	1.3021 0.7680	1.4007 0.71 <i>3</i> 9	2.7028 1.4819	1.2714 0.7866	1.3027 0.7676	2.5741 1.5542	
2.5	1.,450 0.6921	1.6075 0.6221	3.0525 1.3142	1.4046 0.7119	1.5138 0.6606	2.9184 1.3725	1.3701 0.7298	1.4323 0.6982	2.8024 1.4280	1.3336 0.7498	1.3270 0.7536	2.6606 1.5034	

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Table II - Characteristic Slopes Interval 0.4

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Flow fr A Righ B Righ	w from left to right Right up-going characteristic (in degrees) Right down-going characteristic (in degrees)						Ney Slopes refer to characteristics approaching point (A, B)									Key m ₁	$7 \frac{m_1}{1/m_1} \frac{m_2}{1/m_2} \frac{m_1 + m_2}{1/m_1 + 1/m_2}$					
ABI	· • · · · · · · · · · · · · · · · · · ·	2.5			2.9		3.3				3.7			4.1			4.5			4.9		
2.9				1.245 0.803	1.245 0.803	2.490 1.606																
2.5				1.303 0.768	1.266 0.790	2,569 1,558	1.281 0.780	1.210 0.826	2.491 1.606	1.263 0.792	1.159 0.863	2.422 1.655	1.246 0.803	1.113 0.899	2 . 359 1 .7 02	1.231 0.812	1.069 0.935	2.300 1.747	1.217 0.821	1.028 0.972	2.245 1.793	
2,1	1.395 0.717	1.355 0.738	2.750 1.455	1.366 0.732	1.289 0.776	2.655 1.508	1.341 0.746	1.230 0.813	2.571 1.559	1.319 0,758	1.176 0.850	2.495 1.608	1.299 0.770	1.127 0.887	2.426 1.657	1.282 0.780	1.082 0.924	2.364 1.704	1.267 0.789	1.040 0.962	2.307 1.751	
1.7	1.471 0.680	1.387 0.721	2.858 1.401	1.437 0.696	1.316 0.760	2.753 1.456	1.407 0.711	1.253 0.798	2.660 1.509	1.381 0.724	1.196 0.836	2.577 1.560	1.358 0.737	1.144 0.875	2.502 1.612	1.338 0.748	1.096 0.91 <u>3</u>	2.434 1.661	1.320 0.758	1.052 0.951	2 . 372 1.70 9	
1.3	1.559 0.642	1.424 0.702	2,983 1,344	1.517 0.659	1.346 0.743	2.863 1.402	1.481 0.675	1.279 0.782	2.760 1.457	1.450 0.690	1.217 0.821	2.667 1.511	1.422 0.703	1.162 0.860	2.584 1.563	1.398 0.715	1.112 0.899	2.510 1.614	1.377 0.726	1.066 0.938	2•443 1•664	
0.9	1.660 0.603	1.468 0.681	3.128 1.284	1.60B 0.622	1.382 0.723	2.990 1.345	1.564 0.640	1.308 0.765	2.872 1.405	1.526 0.655	1.242 0.805	2.768 1.460	1.494 0.669	1.183 0.845	2.677 1.514	1.465 0.682	1.130 0.885	2.595 1.567	1.440 0.694	1.081 0.925	2.521 1.619	
0.5	1.779 0.562	1.520 0.658	3.299 1.220	1.713 0.584	1.424 0.702	3.137 1.286	1.659	1. <i>3</i> 43 0.745	3.002 1.348	.1.613 0.620	1.271 0.787	2.884 1.407	1.573 0.635	1.208 0.828	2.781 1.463	1.540 0.649	1.150 0.869	2.690 1.518	1.510 0.662	1.099 0.910	2.609 1.572	
0.1	1.923 0.520	1,551 0,645	3.474	1.839 0.544	1.448 0.690	3.287 1.234	1.770 0.565	1.362 0.734	3.132 1.299	1.713 0.584	1.287 0.777	3.000 1.361	1.664 0.601	1.221 0.819	2.885 1.420	1.624 0.616	1.162 0.861	2.786 1.477	1.588 0.630	1.108 0.902	2.696 1.532	
0.1	1.923 0.520	1.520 0.658	3.443	1.839 0.544	1.424 0.702	3.26 3 1.246	1.770	1.343 0.745	3.113 1.310	1.713 0.584	1.271 0.787	2.984 1.371	1.664 0.601	1.208 0.828	2.872 1.429	1.624 0.616	1.150 0.869	2.774 1.485	1.588 0.630	1.099 0.910	2.687 1.540	
0.5	1.779 0.562	1.468 0.681	3.247 1.243	1.713 0.584	1.382	3.095 1.307	1.659 0.603	1.308 0.765	2.967 1.368	1,613 0,620	1.242 0.805	2.855 1.425	1.573 0.635	1.183 0.845	2.756 1.480	1.540 0.649	1.130 0.885	2.670 1.534	1.510 0.662	1.081 0.925	2.591 1.587	
0.9	1.660 0.603	1.424	3.084 1.305	1.608 0.622	1.346 0.743	2.954	1.5 0 4 0.640	1.279 0.782	2.843 1.422	1.526 0.655	1.217 0.821	2.743 1.476	1.494 0.669	1.162 0.860	2.656 1.529	1.465 0.682	1.112 0.899	2.577 1.581	1.440 0.694	1.066 0.938	2.506 1.632	
1.3	1.559	1.387 0.721	2.946 1.363	1.517 0.659	1.316 0.760	2.833 1.419	1.481 0.675	1.253 0.798	2 .73 4 1 . 473	1.450 0.690	1.196 0.836	2.646 1.526	1.422 0.703	1.144 0.875	2.566 1.578	1.398 0.715	1.096 0.913	2.494 1.628	1.377 0.726	1.052 0.951	2.429 1.677	
1.7	1.471	1.355 0.738	2.826	1.437 0.696	1.289 0.776	2.726 1.472	1.407 0.711	1.230 0.813	2.637 1.524	1.381 0.724	1.176 0.850	2.557 1.574	1.358 0.737	1.127 0.887	2.485 1.6 <i>2</i> 4	1.338 0.748	1.082 0.924	2.420 1.672	1.320 0.758	1.040 0.962	2.360 1.720	
2.1	1.395 0.717	1.327	2.722	1.366 0.732	1.266 0.790	2.632	1.341 0.746	1.210 0.826	2.551	1.319 0.758	1.159 0.863	2.478 1.621	1.299 0.770	1.113 0.899	2.412 1.669	1.282 0.780	1.069 0.935	2.351	1.267 0.789	1.028 0.972	2.295	
2.5				1.303 0.768	1.245 0.803	2.548	1,281 0,780	1.193 0.838	2.474 1.618	1.263 0.792	1.144 0.874	2.407 1.666	1.246 0.803	1.099 0.910	2.345 1.713	1.231 0.812	1.057 0.946	2.288 1.758	1.217 0.821	1.019 0.982	2.236 1.803	
2.9							1.227 0.815	1.177 0.850	2.404 1.665	1.211 0.826	1.131 0.884	2.342 1.710	1.196 0.836	1.088 0.920	2.284 1.756	1.183 0.845	1.048 0.955	2.231 1.800	1.172	1.010 0.990	2.182	
3.3						1				1.163 0.860	1.118 0.894	2.281 1.754	1.150 0.869	1.077 0.928	2.227 1.797	1.139 0.878	1.038 0.963	2,177	1.130	1.002	2.132	
3.7						.							1.108 0.903	1.068 0.936	2.176 1.839	1.098	1.030	2.128 1.881	1.090 0.918	0.995	2.085	
4•1																1.060 0.944	1.023	1.921	1.052	0.983	2.041	
4-5																			0.983	1.017	2,000	

Table III - Characteristic Slopes Interval 0.8°

The from left to might

Slopes refer	to	characteristics	approaching	point	(▲,	B)
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A Righ B Righ	rom left it up-goi it down-g	to right ing chara going cha	; acteristi aracteri;	lo (in de stic (in	egrees) degrees))	Slopes refer to characteristics approaching point (A, B) $\frac{1}{m_1} = \frac{m_2}{m_1} = \frac{m_1 + m_2}{m_2} = \frac{1}{m_1 + m_2}$											2 1/m ₂			
A		5.7			6.5			7.3			8,1			8.9			9.7			10.5	· -
2.5	1.200 0.833	0.959 1.043	2.159 1.876																		
1.7	1.296 0.772	0.978 1.023	2 . 274 1.795	1.271 0.787	0.907 1.103	2,178 1,890	1.251 0.799	0,844 1,185	2.095 1.984	1,235 0,810	0.787 1.271	2.022 2.081									
0.9	1.409 0.710	1.001 0.999	2.410 1.709	1.374 0.728	0 . 9 <i>2</i> 4 1.082	2.298 1.810	1.346 0.743	0.857 1.167	2.203 1.910	1.325 0.755	0.797 1.255	2.122 2.010	1.308 0.765	0.743 1.347	2.051 2.112	1.294 0.773	0.693 1.444	1.987 2.217	1.284 0.779	0.647 1.546	1.93 ⁴ 2.325
0.1	1.544 0.648	1.015 0.985	2.559 1.633	1,496 0,669	0.935 1.070	2.431 1.739	1.458 0.686	0.865 1.156	2.323 1.842	1.428 0.700	0.803 1.245	2.231 1.945	1.405 0.712	0.747 1.338	2.152 2.050	1.387 0.721	0.696 1.436	2.083 2.157	1.372 0.729	0.656 1.525	2.028 2.254
0.1	1.544 0.648	1,001 0,999	2.545 1.647	1.496 0.669	0 . 924 1.082	2.420 1.751	1.458 0.686	0.857 1.167	2.315 1.853	1.428 0 .70 0	0.797 1.255	2.225 1.955	1.405 0.712	0.743 1.346	2.148 2.058	1.387 0.721	0.693 1.444	2.080 2.165	1.372 0.729	0.647 1.546	2.019 2.275
0.9	1.409 0.710	0.978 1.023	2.387 1.733	1.374 0.728	0.907 1.103	2.281 1.831	1.346 0.743	0.844 1.185	2.190 1.928	1.325 0.755	0.787 1.271	2.112 2.026	1.308 [°] 0.765	0.735 1.361	2.043 2.126	1.294 0.773	0.687 1.456	1.981 2.229	1.284 0.779	0.643 1.556	1.927 2.335
1.7	1.296 0.772	0.959	2.255 1.815	1.271 0.787	0.893 1.120	2.164	1.251 0.799	0.833	2.084 1.999	1.235 0.810	0.779 1.284	2.014 2.094	1.222 0.818	0.729 1.372	1.951 2.190	1.213 0.825	0.683 1.464	1.896 2.289	1.206 0.829	0.640 1.562	1.846 2.391
2.5	1.200 0.833	0.944 1.059	2.144 1.892	1.182 0.846	0.882 1.134	2.064 1.980	1.167 0.857	0.825 1.213	1.992 2.070	1.155 0.866	0.773 1.294	1.928 2.160	1.146 0.873	0.725 1.380	1.871 2.253	1.140 0.878	0.680 1.470	1.820 2.348	1.135 0.881	0.638 1.566	1.773 2.447
3.3	1.117 0.895	0.933 1.072	2.050 1.967	1.103 0.907	0.873 1.146	1.976 2.053	1.092 0.916	0.818 1.222	1.910 2.138	1.083 0.923	0.768 1.302	1.851 2.225	1.077 0.928	0.722 1.385	1.799 2.313	1.073 0.932	0.679 1.474	1.752 2.406	1.071 0.934	0.638 1.568	1.709 2.502
4.1	1.043 0.959	0.923 1.083	1.966 2.042	1.032 0.969	0.866 1.155	1.898 2.124	1.024 0.976	0.814 1.229	1.838	1.019 0.982	0.765	1 .7 84 2.289	1. 015 0.985	0.720 1.388	1.735 2.373	1.013	0.678 1.475	1.691 2.462	1.012 0.989	0.638 1.567	1.650 2.556
4.9	0.976 1.024	0.916 1.092	1.892 2.116	0.969 1.032	0.861 1.161	1.830 2.193	0.963 1.038	0.810 1.234	1.773	0.960 1.042	0.763	1.723 2.352	0.958 1.044	0.719 1.390	1.677 2.434	0.957 1.045	0.678 1.474	1.635 2.519	0.957 1.045	0.639 1.564	1.596 2.609
5.7				0.911 1.098	0.858 1.166	1.769 2.264	0.907	0.809 1.237	1.716 2.339	0.905 1.104	0.763 1.310	1.668 2.414	0.905 1.106	0.720 1.388	1.625 2.494	0.905 1.105	0.679 1.472	1.584 2.577	0.906	0.641 1.559	1.547 2.662
6.5							0.856 1.168	0.808 1,238	1.664 2.406	0.855 1.170	0.763 1.310	1.618 2.480	0.855 1.169	0.721 1.387	1.576 2.556	0.857 1.167	0.681 1.468	1.538 2.635	0.859 1.164	0.644 1.553	1.503 2.717
7.3										0.808 1.237	0.764 1.308	1.572 2.545	0.809 1.235	0.723 1.383	1.532 2.618	0.812 1.232	0.684 1.462	1.496 2.694	0.815 1.227	0.647 1.545	1.462 2.772
8.1													0.766 1.305	0.726 1.377	1.492 2.682	0.770 1.299	0.688 1.454	1.458 2.753	0.773	0.651 1.536	1.424 2.829
8.9																0.729 1.371	0.691 1.446	1.420 2.817	0.734 1.363	0.655 1.526	1,389 2,889
9 .7																			0.696 1.437	0.660 1.514	1.356 2.951

Slopes refer to characteristics approaching point (A, B)

Flow from left to righ: A Right up-going characteristic (in degrees) B Right down-going characteristic (in degrees)

A	12.1			13.7			1	15.3		1	16.9		<u> </u>	18.5			20.1		21.7		
0.9	1.274 0.785	0.564 1.773	1.838 2.558	1.268 0.789	0.491 2.038	1.759 2.827															
0.1	1.357 0.7 <i>3</i> 7	0.565 1.770	1.922 2.507	1.346 0.743	0.491 2.038	1.837 2.781	1.343 0.744	0.424 2.360	1.767 3.104	1.348 0.742	0.362 2.759	1.710 3.501	1.358 0.736	0,305 3,274	1.663 4.010	1.374 0.728	0.2519 3.969	1.626 4.697			
0.1	1.357 0.737	0.564 1.773	1.921 2.510	1.346 0.743	0.491 2.038	1.837 2.781	1.343 0.744	0.424 2.360	1.767 3.104	1.348 0.742	0.364 2.750	1.712 3.492	1.358 0.736	0.307 3.258	1.665 3.994	1.374 0.728	0.254 3.940	1.628 4.668	1.394 0.717	0.203 4.917	1.597 5.634
0.9	1.274 0.785	0.562 1 .7 79	1.836 2.564	1.268 0.789	0.491 2.035	1.759 2.824	1.269 0.768	0.4 <i>2</i> 7 2.342	1.696 3.130	1.276 0.784	0.368 2.720	1.644 3.504	1.288 0.776	0.312 3.203	1.600 3.979	1.301 0.766	0.260 3.846	1.561 4.612	1.326 0.754	0.210 4.753	1.536 5.507
2.5	1.132 0.883	0.563 1.777	1.695 2.660	1.133 0.883	0,495 2.022	1.628 2.905	1.139 0.878	0.432 2.313	1.571 3.191	1.150 0.870	0.375 2.669	1.525 3.539	1.164 0.859	0,321 3,120	1.485 3.979	1.182 0.846	0.269 3.711	1.451 4.557	1.204 0.831	0,221 4,531	1.425 5.362
4.1	1.013 0.987	0.566 1.776	1.579 2.753	1.018 0.982	0.500 1.998	1.518 2.980	1.028 0.973	0.440 2.274	1.468 3.247	1.041 0.961	0.383 2.608	1.4 <i>2</i> 4 3.569	1.057 0.946	0.330 3.027	1.387 3.973	1.075 0.930	0.280 3.571	1.355 4.501	1.097 0.912	0.232 4.308	1.329 5.220
5.7	0.911 1.098	0.572 1.747	1.483 2.845	0.919 1.088	0.508	1.427 3.056	0.931 1.075	0.449 2.228	1.380 3.303	0.945 1.058	0.394 2.541	1.339 3.599	0.962	0.341 2.929	1.303 3.969	0.981 1.020	0.292 3.427	1.273 4.447	1,002 0,998	0.244 4.090	1.246 5.088
7.3	0,821 1,218	0.581 1.722	1.402 2.940-	0.831 1.203	0.518 1.931	1.349 3.134	0.844 1.184	0.460 2.176	1.304 3.360	0.860 1.163	0.405 2.469	1.265 3.632	0.877 1.140	0.354 2.829	1.231 3.969	0.896 1.116	0.305 3.283	1.201 4.399	0.918 1.090	0.258 3.880	1.176 4.970
8.9	0.741 1.349	0.591 1.692	1.332 3.041	0.753 1.328	0.529 1.890	1.282 3.218	0.767 1,304	0.472 2.121	1.239 3.425	0.783 1.278	0.418 2.394	1.201 3.672	0.800 1.250	0.367 2.727	1.167 3.977	0.820 1.220	0.318 3.142	1.138 4.362	0.841 1.190	0.272 3.679	1.113 4.869
1 0.5	0.669 1.495	0.603 1.659	1.272 3.154	0.682 1.467	0.542 1.846	1.224 3.313	0.696 1.436	0 . 485 2 .0 62	1.181 3.498	0.712 1.404	0.431 2.318	1.143 3.722	0.730 1.369	0.381 2.625	1.111 3.994	0.750 1.334	0.333 3.005	1.083 4.339	0.770 1.298	0.287 3.488	1.057 4.786
12.1				0.616	0.556	1.172 3.421	0.631 1.584	0.499 2.002	1.130 3.586	0.648 1.543	0.446 2.240	1.094 3.783	0.666 1.502	0•396 2•525	1.062 4.027	0.685 1.460	0.348 2.872	1.033 4.332	0.705 1.418	0.302 3.308	1.007 4.726
13.7	:						0.571 1.750	0.515 1.941	1.086 3.691	0.588 1.701	0.462 2.163	1.050 3.864	0.606 1.651	0.412 2.426	1.018 4.077	0.625	0.364 2.744	0.989 4.344	0.645 1.551	0.319 3.138	0.964 4.689
15.3										0.532 1.880	0.479 2.088	1.011 3.968	0.550 1.819	0.429 2.331	0.979 4.150	0.568 1.759	0.381 2.622	0.949 4.381	0.588 1.700	0.336 2.979	0.924 4.679
16.9													0.497 2.013	0.447 2.238	0.944 4.251	0.515 1.940	0.399 2.506	0.914 4.446	0.535 1.869	0.353 2.830	0.888 4.699
18.5																0•465 2•149	0.417 2•395	0.882 4.544	0.485 2.063	0.372 2.690	0.857 4.753
20.1																1			0.437 2.290	0.391 2.559	0.828 4.849

•	^m 1	^m 2	m ₁ +	^m 2
ļ	1/=1	1/m 2	1/m1	+ 1/m2

Flow from left to right A Right up-going characteristic (in degrees) B Right down-going characteristic (in degrees)

Key m

Bloces refer to characteristics approaching point (A, B)

1/m

La Late L		B 23.3		24.9		26.5		28.1		29.7			31.3			32+9			<u> </u>	54.5			76.1					
D D	0.	1 1.41	86 0.155	1 1.5737	1.4472	0.1085	1.5557	1.4799	0,0635	1.5434	1.5165	0.0194	1.5359	1.5572	-0.0238	1.5334	1.6019	-0.0564	1.5355	1 6511	-0.1090			1 24.5	1		36.1	
50 6100 6	0	0.70	5 6,448	7.153	0.691	9.210	9.901	0.676	15.75	16-43	0.659	51.47	52.13	0.642	-42,05	-41.42	0.624	-15.06	-14.44	0.606	-9.205	-8.599						
15 1		0.74	0 6.143	6.883	0.725	8-554	9.279	0.709	13.82	1.4530	1.4463 0.691	0.0309 34.66	1+4752 35+35	1.4856	-0.0139	1.4717 -71.58	1.5286 0 654	-0,0560 -17,87	1.4726 -17.22	1.5755 0.635	-0.0977 -10.236	1.4778 -9.601						
1 1	2.	5 1.22 0.81	62 0.1739 6 5-749	1.4021 6.563	1.2557 0.796	0.1288 7.766	1.3845 8.562	1.2864 0.777	0.0849 11.78	1.3713 12.56	1.3200 0.758	0.0420 23.79	1.3620 24.55	1.3567 0.737	-0.0001	1.3568 -19, 398	1.3967	-0.0415	1.3552 23.34	1.4399 0.694	-0.0827 -12.09	1.3572						
5.57 1.600	4.	1 1.12	11 0.1860 2 5.375	1.3071 6.267	1.1479 0.871	0-1415	1.2894 7.939	1.1772	0.0982	1.2754	1.2091	0.0558	1.2649 18.74	1.2436	0.0143	1.2579	1.2809	-0.0267	1.2542	1.3209	-0.0672	1.2537	1.3640	-0.1076	1.2564	1.4102	-0.1479	1.2623
1 1	5.	7 1.02	51 0.1990 5 5.026	1.2251	1.0521	0.1549	1+2070	1.0802	0.1121	1-1923	1.1105	0.0703	1.1808	1.1431	0.0292	1.1723	1.1781	-0.0113	1.1658	1.2154	-0+0514	1.1640	1.2554	-9.296	1.1642	0.7091 1.3125	-6.764	-6+055
1 0 0 0 5 5 5 5 0	7.	3 0.94	8 0.2127	1-1535	0.9659	0.1690	1.1349	0.9929	0.1267	1.1196	1.0219	0.0852	15-13	1+0528	0.0446	35-12 1-0974	1.0858	-88.69	-87.84	0.823	=19.47	=18+65	0.7966	-10.967	-10.170	0.7621	-7.640	-6-878
1.12 4.46 5.55 1.125 5.60 1.125 5.105 1.020 1.0	8.	9 0.863	4.702 4 0.2271	5.765	1.035	5-914 0-1839	6.949	1.007	7.894 0.1418	8-901	0.979	11-75	12.71	0.950	22.42	23.37	0.921	220.4	221.3	0.892	-28.49	-27.60	0.8635	-13-43	-12.57	0.8349	-0.1137	-7-960
1.100 1.100 1.100 0.2009 0.4009 <th>10-</th> <th>1.15</th> <th>4.403</th> <th>5-561</th> <th>1.126</th> <th>5.438</th> <th>5.564</th> <th>1+094</th> <th>7.050</th> <th>8.144</th> <th>1.062</th> <th>9.925</th> <th>10.987</th> <th>1.030</th> <th>16.54</th> <th>17.57</th> <th>0.998</th> <th>48.14</th> <th>1.0228 49.14</th> <th>1,0352 0,966</th> <th>-0.0185 -54.15</th> <th>1.0167 =53.18</th> <th>1.0702</th> <th>-0.0574 -17.42</th> <th>1.0128</th> <th>1.1072 0.9032</th> <th>-0.0962</th> <th>1.0110</th>	10-	1.15	4.403	5-561	1.126	5.438	5.564	1+094	7.050	8.144	1.062	9.925	10.987	1.030	16.54	17.57	0.998	48.14	1.0228 49.14	1,0352 0,966	-0.0185 -54.15	1.0167 =53.18	1.0702	-0.0574 -17.42	1.0128	1.1072 0.9032	-0.0962	1.0110
11 11<		1.262	4.128	5.390	1.225	5,017	6.242	1.189	0.1576 6.347	0.9989 7.536	0.8679 1.152	0.1168 8.565	0.9847 9.717	0.8960 1.116	0.0767 13.03	0.9727 14.15	0.9257 1.080	0.0374 26.74	0.9631 27.82	0.9570 1.045	-0.0015 -668.4	0.9555 -667.4	0.9901 1.0100	-0.0401 -24.94	0.9500 -23.93	1.0248 0.9758	-0,0785 -12,75	0.9463 -11.77
10.7 0.682 0.3786 0.6878 0.4878 0.4887 0.4887 0.4877 0.4983 0.4984 0.4897 0.4794 0.4994 <th>12.</th> <th>1 0.727</th> <th>0 0.2581 3.874</th> <th>0.9851 5.249</th> <th>0.7501 1.333</th> <th>0.2154 4.643</th> <th>0.9655 5-976</th> <th>0.7744 1.291</th> <th>0.1738 5.754</th> <th>0.9482 7.045</th> <th>0.8000 1.250</th> <th>0.1332 7.505</th> <th>0.9332 8.755</th> <th>0.8270 1.209</th> <th>0.0935 10.695</th> <th>0.9205 11.904</th> <th>0.8553 1.169</th> <th>0.0544 18.38</th> <th>0.9097 19.55</th> <th>0.8852 1.130</th> <th>0.0158 63.38</th> <th>0.9010 64.51</th> <th>0.9164 1.0912</th> <th>-0.0225</th> <th>0.8939</th> <th>0.9494 1.0533</th> <th>-0.0633</th> <th>0.8861 -15.48</th>	12.	1 0.727	0 0.2581 3.874	0.9851 5.249	0.7501 1.333	0.2154 4.643	0.9655 5-976	0.7744 1.291	0.1738 5.754	0.9482 7.045	0.8000 1.250	0.1332 7.505	0.9332 8.755	0.8270 1.209	0.0935 10.695	0.9205 11.904	0.8553 1.169	0.0544 18.38	0.9097 19.55	0.8852 1.130	0.0158 63.38	0.9010 64.51	0.9164 1.0912	-0.0225	0.8939	0.9494 1.0533	-0.0633	0.8861 -15.48
15.5 6.603 6.916 6.9020 6.9176 6.9026 6.9796 6.9027 6.918 6.9026 6.9796 6.928 6.9796 6.9797 6.9796 6.9796 6.9797 6.9796 6.9796 6.9797 6.9796 6.9797 6.9796 6.9797 6.9796 6.9797 6.9796 6.9797 6.9797 6.9796 6.9797 6.9796 6.9797 6.9796 6.9797 6.9796 6.9797 6.9796 6.9797 6.9797 6.9797	13.	7 0.666 1.501	2 0.2746 3.641	0.9408 5.142	0•6887 1•452	0.2320 4.311	0.9207 5-763	0.7122 1.404	0, 1906 5-247	0.9028 6.651	0.7370 1.357	0. 1902 6. 658	0.6872 8.015	0,7630 1,311	0.1107 9.038	0.8737 10.349	0.7902 1.266	0.0717 13.94	0.8619 15-21	0.8186	0.0334 29.94	0.8520 31.16	0-8485	-0.0046	0.8439	0.8797	-0.0423	0.8374
16.0 0.5957 0.4957	15.3	5 0.609 1.641	3 0.2916 3.429	0.9009 5.070	0.6312 1.584	0.24 9 1 4.014	0 . 8803 5.598	0.6541 1.529	0.2079	0.6620 6.340	0.6781 1.475	0. 1576 5.967	0.8457	0,7032 1.422	0.1282	0.8314	0.7293	0.0895	0.8188	0.7566	0.0513	0.6079	0.7852	0.0136	0.7988	0.8150	-0.0238	0.7912
10-5 0.5904 0.3277 0.6328 0.4291 1.437 1.439 1.437 1.439 1.437 1.439 1.437 1.439 1.437 1.439 1.437 1.439 1.437 1.439	16.9	0.555	7 0.3094 3.232	0.8651 5.032	0,5772 1.733	0.2668 3.747	0.8440 5.480	0-5995	0.2256	0,8251	0.6228	0. 1854 5 304	0.8082	0.6470	0.1461	0,7931	0.6723	0.1075	0.7798	0.6986	0.0695	0.7681	0.7259	0.0320	74-81 0 - 7579	0.7545	-0.0052	⊷40.68 0.7493
Instruction Jobs Loss	18.	5 0.504	0.3277	0.8326	0-5299	0.2851	0.8110	0-5478	0.2439	0.7917	0.5705	0,2037	0.7742	0.5941	0.1644	0.7585	0.6185	9.299 0.1259	10.786 0.7444	1.431 0.6440	14.38 0.0881	15.81 0.7321	1•3775 0•6703	31+25 0+0507	32.63 0.7210	1 -3254 0-6976	-191.7 0.0137	-190.4
2.190 2.266 5.076 2.695 3.200 5.88 2.005 3.100 5.417 1.497 6.477 6.476 6.476 6.476 6.476 6.492 6.476 6.476 6.496 6.497 6.476 6.497 6.476 6.497 6.497 6.476 6.497 6.476 6.497 6.476 6.497 6.476 6.497 6.497 6.476 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.497 6.498 6.497 6.497 6.498 6.497 6.498 6.497 6.497 6.498 6.497 6.498 6.497 6.498 6.497 6.498 6.498 6.498 6.498 6.498 6.498 6.498 6.497 6.498 6.497 6.498 6.497 6.498 6.497 6.498 6.498 6.498 6.498 6.498 6.498 6.498 6.498 6.498 6.498 6.498 6.498 6.498 <th6.498< th=""> 6.498 <th6.< th=""><th>20.1</th><th>0.456</th><th>5 0.3466</th><th>0.8032</th><th>0.4773</th><th>0.3038</th><th>0.7811</th><th>0.4987</th><th>4.101 0.2626</th><th>5.926 0.7613</th><th>1+753 0+5209 </th><th>4.909</th><th>6.662 0.7433</th><th>1.683 0.5438</th><th>6.082</th><th>7•765 0-7269</th><th>1.617</th><th>7.941</th><th>9.558</th><th>1-555</th><th>11.356</th><th>12,909</th><th>1.4919</th><th>19.73</th><th>21.22</th><th>1.4334</th><th>73.17</th><th>74.60</th></th6.<></th6.498<>	20.1	0.456	5 0.3466	0.8032	0.4773	0.3038	0.7811	0.4987	4.101 0.2626	5.926 0.7613	1+753 0+5209	4.909	6.662 0.7433	1.683 0.5438	6.082	7•765 0-7269	1.617	7.941	9.558	1-555	11.356	12,909	1.4919	19.73	21.22	1.4334	73.17	74.60
2.437 2.732 5.169 2.322 3.994 5.4169 0.4375 0.4495 0.4415 0.4594 0.4994 0.4795 0.4495 0.4495 0.4415 0.4595 0.4495 0.4415 0.4395 0.4495 0.4415 0.4395 0.4495 0.4415 0.4395 0.4495 0.4415 0.4395 0.4495 0.4415 0.4395 0.4435 0.4495 0.4416 0.4495 0.4416 0.4495 0.4416 0.4495 0.4416 0.4495 0.4416 0.4416 0.4416 0.4416 0.4416 0.4416	21.7	2.190	2,586	5-076 0.7764	2.095 0.4308	3.290 0.3232	5-385 0-7540	2.005	3.808	5-813	1.920	4.497	6.417	1-839	5.461	7.300	1.762	6.912	8.674	1.689	9-356	11.045	1.6190	0.0696 14.36	0.6872 15.98	0.6441 1.5527	0.0326 30.53	0.6768 32.08
2.50 0.362 0.331 0.7333 0.4223 0.4221 0.4221 0.477 0.1822 0.4950 0.4744 0.1280 0.4924 0.4950 0.4744 0.1280 0.4924 0.4950 0.4744 0.1280 0.4744 0.1280 0.4950 0.4744 0.1280 0.4744 0.1280 0.4744 0.1280 0.4990 0.4990 0.4744 0.1280 0.4744 0.1280 0.4744 0.1280 0.4744 0.1280 0.4744 0.1280 0.4744 0.1280 0.4744 0.1280 0.4744 0.1280 0.4746 0.4744 0.1280 0.4746 0.4596 0.4747	23.3	2.437	2.732	5-169	2.322	3.094	5.416	2,213	3.549	5-762	2.112	4.141	0.7150 6.253	0.4959 2.016	0.2022 4.945	0, 6981 6,961	0.5191 1.926	0.1638 6.106	0.6829 8.032	0.5430 1.842	0.1260 7.934	0.6690 9.776	0.5677 1.7615	0.0888 11.259	0.6565 13.020	0•5932 1•6858	0.0521 19.21	0.64 <u>5</u> 3 20.90
24.9 0.3630 0.3217 0.6693 0.3845 0.4281 0.4665 0.4245 0.4295					2.590	2.914	0.7293 5.504	0,4068 2,4 <u>5</u> 8	0.3015 3.317	0.7083 5+775	0,4282 2.336	0.2611 3.830	0.6893 6.166	0.4501 2.222	0.2217 4.511	0.6718 6.733	0.4727 2.115	0.1832 5.458	0.6559 7•573	0.4960 2.016	0.1455 6.875	0.6415 8.891	0.5201 1.9230	0•1083 9•235	0.6284 11.158	0.5448 1.8357	0.0716 13.97	0.6164 15.80
26.5 0.3624 0.3677 0.2618 0.6255 0.3854 0.2231 0.6065 0.4077 0.1852 0.4306 0.1480 0.5786 0.4500 0.1114 0.5654 28.1 2.921 3.516 6.237 2.750 3.818 6.568 2.935 4.481 7.076 2.433 5.398 7.051 2.3226 6.756 0.4500 0.1114 0.5654 28.1 0.3225 0.2828 0.2825 0.2828 0.6051 0.3439 0.2437 7.0676 2.453 0.5714 0.3083 0.5680 0.4113 0.1114 0.5600 29.7 3.100 3.539 0.2826 0.6051 0.3439 0.2437 7.056 2.5757 5.941 0.5517 2.4316 7.596 0.5714 0.3803 0.1633 0.5565 0.4113 0.1114 0.5200 29.7 3.103 3.599 0.2826 0.5976 0.2683 0.2237 0.5976 0.2686 0.5971 0.3473 0.1800 0.5163 0.3699 0.1521 0.5200 31.3 3.498 0.2247	24.9							0.3636 2.750	0.3217 3.109	0.6853 5-659	0.3845 2.601	0.28tt 3.556	0.6656 6.159	0 .4061 2.463	0.2416 4.1 <i>3</i> 9	0.6477 5.602	0.4283 2.335	0.2031 4.926	0.6314	0.4510 2.217	0.1651	0.6161	0.4744	0.1280 7.811	0,6024 9,919	0.4985 2.0061	0-0914	0.5899
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	26.5					ļ					0 . 3424 2.921	0.3016 3.316	0,6440 6,237	0.3637 2.750	0.2618	0.6255	0.3854	0.2231	0.6085	0-4077	0.1852	0,5929 7.851	0.4306	0.1480	0.5786	0.4540	0.1114	0.5654
29.7 31.3 - </th <th>28.1</th> <th></th> <th>0.3225</th> <th>0.2826</th> <th>0.6051</th> <th>0,3439</th> <th>0.2437</th> <th>0,5876</th> <th>0.3658</th> <th>0.2056</th> <th>0.5714</th> <th>0.3883</th> <th>0.1683</th> <th>9.079 0.5566</th> <th>0.4113</th> <th>0.1317</th> <th>0.5430</th>	28.1													0.3225	0.2826	0.6051	0,3439	0.2437	0,5876	0.3658	0.2056	0.5714	0.3883	0.1683	9.079 0.5566	0.4113	0.1317	0.5430
$3.29^{2} 3.780 7.072 3.074 4.418 7.492 2.879 5.293 8.172 2.7037 6.573 9.276$ $3.29^{2} 3.780 7.072 3.074 4.418 7.492 2.879 5.293 8.172 2.7037 6.573 9.276$ $3.29^{2} 3.498 4.042 7.540 3.251 4.766 8.017 3.033 5.783 8.816$ $32.9 34.5 34.5 3.719 4.327 8.046 3.440 5.155 8.995$	29.7				ļ								ľ	5.100	3.539	6 .63 9	2•907 0•3037	4.103	7.010	2.733	4.863	7•596 0-5517	2•5757	5-941 0.1890	8.517	2,4316	7.598	10.030
32.9 34.5	31.3																3.292	3.780	7.072	3.074	4.418	7-492	2.879	5-293	8.172	2.7037	6.573	9-276
34.5 34.5	32.9			ļ																0.2859 3.498	4.042	0.5334 7.540	0.3076 3.251	0.2098 4.766	0.5174 8.017	0.3298 3.033	0.1729 5.783	0.5027 8.815
0.2526 0.2141 0.4667 3-958 4.671 8.629	34.5																	ļ					0.2689 3.719	0.2311 4.327	0,5000 8,046	0.2907 3.440	0.1940 5-155	0.4847 8-595
																						ł		Í		0.2526 5-958	0.2141 4.671	0.4667 8.629

$$m_2 m_1 + m_2$$

 $m_1 1/m_2 1/m_1 + 1/m_2$

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FIG. I. SKETCH OF CHARACTERISTICS INTERSECTIONS.



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