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Low Altitude Gust Measurements over Three Routes in the U.K.

By E. W. Wells

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C.P. No. 676

October, 1962

LOW ALTITUDE GUST MEASUREMENTS OVER THREE ROUTES IN THE U.K.

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E. W. Wells

SUMMARY

A number of flights have been made at low altitude over three routes in the U.K. The routes were in Sussex. East Anglia and Wales. Measurements made with a counting accelerometer have been analysed to investigate the effect of variation in terrain and meteorological conditions on the intensity of turbulence. A comparison has also been made between these flights and flights made at low altitude in North Africa.

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1 INTRODUCTION

During the period September 1959 to February 1962 a number of flights were made at low altitude over three routes in the United Kingdom. The object of the experiment was to assess the intensity of turbulence at low altitude and its variation with differences in terrain and meteorological conditions. The flights were made in a Canberra aircraft and the normal acceleration levels exceeded were counted by means of a counting accelerometer near the centre of gravity of the aircraft and converted to equivalent gust velocities by using the discrete gust analysis¹.

2 DETAILS OF ROUTES

The three routes over which the flying took place are shown on Fig.1. The first was in Sussex between Petersfield and Bodiam a distance of 64 miles. This route started over hilly wooded country of the South Downs and later passed over flatter country consisting of a mixture of fields, woods, farms and villages typical of the Sussex Weald.

The second route was in East Anglia between the airfields of Waterbeach and Coningsby. The run was 56 miles in length and passed over flat fen country, which was cultivated in the South and marshy at the Northern end.

The third route was in Wales between Glasbury and Berriew; it was 38 miles in length and lay over open hilly country with peaks rising to approximately 2000 feet above sea level.

A contour of the ground along each route is shown on Fig.2.

3 AIRCRAFT, INSTRUMENTATION AND FLIGHT TECHNIQUE

The aircraft used was a standard Canberra B6. A R.A.E. Compound Counting Accelerometer Mk.4 installed near the aircraft centre of gravity was used to count the normal accelerations levels experienced by the aircraft. Details of the aircraft and accelerometer are given in Appendix 1.

For determining the temperature lapse rate during flight a Meteorological Office Balanced Bridge Thermometer was installed in the aircraft, the element being fitted under the nose. For the early flights the temperature was obtained by reading the Indicator, but on flights made after 1959 the output of the bridge was fed into a Beaudouin A13 recorder and the temperature was continuously recorded.

The flying extended over a period of approximately $2\frac{1}{2}$ years and was part of a larger programme investigating loads due to gusts on aircraft. The flights were made at irregular intervals throughout each year and under varying meteorological conditions. On each flight the route being examined was flown a number of times in each direction, usually a sufficient number to bring the recording time up to approximately 30 minutes. The accelerometer counters were switched on at the start and off at the end of each run so that loads caused by the aircraft turning between runs were not recorded. The aircraft was flown at approximately 200 feet above the ground and an attempt was made to follow the ground contours, hereafter referred to as "contouring".

4 METEOROLOGICAL INFORMATION

Information on the state of the weather for each flight was obtained from the nearest hourly observations made at Gatwick for the Sussex flights, Rhayader for the Welsh flights, and Waterbeach and Coningsby for the flights in East Anglia (positions shown on map, Fig.1). The information supplied by each station was as follows:-

- 4 -

Surface wind speed and direction Visibility Cloud type and amount Soreen temperature Dew point.

A summary of the average meteorological information for the period of each flight is given in Table 1.

An average temperature lapse rate was obtained for each flight over the height band 200 ft to 1000 ft above ground from a thermometer carried externally on the aircraft. Details of the method of measurement are given in Appendix 1.

5 CONVERSION OF ACCELERATION COUNTS TO GUST VELOCITIES

The normal acceleration levels were converted to equivalent gust velocity levels by means of the discrete gust procedure described in Ref.1. The computation was done on a Deuce computer by the method described in Ref.2.

6 RESULTS

In Table 2 are listed details of all the flights showing the number of gusts recorded and the number of gusts per mile. The number of gusts given in Table 2 is the total obtained when the number of occurrences of up and down gusts at equal levels of gust velocity are added together.

Table 3 lists separately the numbers of up gusts and of down gusts recorded during each of the flights.

The average gust spectra for each route are shown on Fig.3. From this Figure it will be seen that the Welsh route produced the largest number of occurrences at the higher levels of gust velocity. This is to some extent due to the inclusion of the loads produced by the pilot "contouring" over the hilly ground along the route.

6.1 Sussex

Fig.4 shows the relationship between occurrences per mile of gusts of 5 ft/sec or greater and wind speed for the Sussex route. There is a correlation between gust intensity and wind speed. The results have also been grouped in ranges of wind speed for four ranges of temperature lapse rate. They are listed in Table 4 and shown plotted on Fig.5. Again the results show correlation between gust intensity and wind speed. The Figure also shows that lapse rate is an important factor and that the difference in the degree of turbulence between the two extreme ranges of lapse rate, one stable and the other unstable, is marked.

Plotting the number of gusts per mile of 5 ft/sec or greater against lapse rate (Fig.6) again shows some correlation, especially for the higher values of wind speed. Grouping the data in ranges of wind speed gives Table 5 and the results are shown plotted on Fig.7. This clearly shows a relationship with lapse rate becoming most marked at the higher wind speeds.

6.2 East Anglia

The number of gusts per mile of 5 ft/sec or greater is plotted against wind speed on Fig.8 and against lapse rate on Fig.9. The results were too few to allow separation of the effects of wind speed and lapse rate. Separation was moreover made impractical by the fact that on the occasions when flights were made, high winds were associated with high lapse rates and low wind speeds with low lapse rates.

6.3 Wales

The results from this route, due to the hilly nature of the terrain, include a considerable effect from loads due to "contouring". Also fewer flights were made over this route making it more difficult to draw conclusions from the results. By comparing the results against wind speed however (Fig.10) there appears to be a significant trend of increasing turbulence with inoreasing wird speed, but no trend can be observed with lapse rate (Fig.11).

6.4 Comparison between the Sussex and East Anglian Routes

An attempt has been made to examine the variation in the gust spectra due to the difference in the type of terrain. The comparison has been restricted to the Sussex and East Anglian routes, the results from these routes being less affected by "contouring" loads than those from the Welsh route.

The average figure for the number of gusts per mile for six flights over the Sussex route and six over the East Anglian route, when the wind speed and lapse rate were within a limited range, was obtained. Each group of six flights was made on days when the wind was in the range of 11 to 16 kts and the lapse rate 2.0 to 3.1° C/1000 ft. The two sets of results are shown plotted on Fig.12. The flat terrain along the East Anglian route produced fewer gusts than the more hilly and varied terrain of the Sussex route.

6.5 Comparison between U.K. and North Africa

A comparison has been made between the gust spectra measured on the U.K. routes with those measured in North Africa during the 'Swifter' experiment³.

The results for all the flying on each of the three U.K. routes have been compared with those obtained in North Africa in the most severe conditions, namely, midday flights over the hilly desert leg. An average gust spectrum for the whole year was taken for the North African flying and also an average spectrum for the three summer months of June, July and August, when the turbulence was more severe thar in other months. The results are shown plotted on Fig.13.

It will be seen that the average gust intensity even for the three summer months is not significantly higher than the average for all the flying on the Sussex route. The U.K. flights tended to be carried out on days when turbulence was expected although this was not always the case. The flights cover a large range of wind speed and lapse rate and they were made during all months of the year. It is also significant that the largest figure obtained on any flight for the total number of occurrences per mile of gusts of 5 ft/sec or greater was approximately 13 during the North African flying, compared with a figure of 17 obtained during a flight along the Sussex route⁴.

^{*} Comparative gust measurements were made on a B.2 and B.6 Canberra in North Africa to establish that differences were not due to the different marks of Canberra used in North Africa and U_2K_2

7 CONCLUSIONS

The results from the three routes in the U.K. are as follows:-

(i) Over a varied terrain consisting of a mixture of low hills, woods and farmland, as found in Sussex, both wind speed and temperature lapse rate were found to be significant factors in producing turbulence. The effect of lapse rate increased with increase in wind speed.

(ii) It was not possible to distinguish between the effects of wind speed and temperature lapse rate over the flat terrain of East Anglia due to the limited amount of flying carried out over this route. Unfortunately, high temperature lapse rates occurred when high wind speeds were present and low lapse rates were associated with low wind speeds.

(iii) Over the hilly terrain of Wales, wind speed appeared to be a significant factor in producing turbulence, but the results from this region were affected by the loads caused by following the contours of the hills.

For a given value of wind speed and lapse rate there was found to be significantly more turbulence over the undulating, varied terrain of Sussex than over the flat terrain of East Anglia.

The intensity of turbulence at low altitude over Southern England was comparable with that measured over the hilly desert of North Africa.

LIST OF REFERENCES

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1	Zbrozek, J.K.	Gust alleviation facto A.R.C. R.& M. 2970.	ors. August, 1953.
2	Heath Smith, J.R.	The estimation of atmo frequencies from count records using the Deuc R.A.E. Tech. Note No. A.R.G. 20,921.	ospheric gust ting accelerometer ce computer. Structures 240, October, 1958.
3	Bullen, N.I.	Gusts at low altitude	in North Africa.
		A.R.C. C.P.581.	September, 1961.

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APPENDIX 1

DETAILS OF AIRCRAFT AND INSTRUMENTATION

1 The aircraft used in the tests was a standard Canberra B.6, having an all-up-weight at take-off of 43,000 lbs. Other aircraft characteristics are:-

Wing span	64 feet
Mean chord	15 feet
Gross wing area	960 sq.ft.
Aspect ratio	4.25
Slope of lift curve	3.6 per radian

The R.A.E. Counting Accelercmeter Mk.4 carried on the aircraft records the number of times that the normal acceleration has exceeded the following levels of absolute acceleration:-

Levels > 1.0g level flight condition 1.2 1.3 1.4 1.6 1.8 2.0 2.2 2.4 2.6g Levels < 1.0g level flight condition 0.9 0.8 0.7 0.6 0.4 0.2 0 -0.2 -0.4 -0.6g

Further details of the characteristics of the accelerometer are given in Ref.2.

The instrument also contained an airspeed indicator, a clock and, instead of the standard pressure altimeter, a milliammeter connected into the radio altimeter circuit suitably calibrated to indicate the height of the aircraft above ground. Arrangements were made for the acceleration counters to be switched on at the start of a run by an observer in the aircraft. The camera would then commence taking a picture of the counter readings, airspeed, height above ground and time every minute until the end of the run when the observer would switch the counters off. The camera would then take one more picture at the completion of the minute during which the counters were switched off.

Notes on the aircraft fuel state were made by the observer at intervals during the runs.

On flights before 31st May 1960 the lapse rate was obtained by making a run at 1000 ft above ground between two of the 200 ft runs and measuring the outside air temperature by means of a Meteorological Office Balanced Bridge Thermometer at one minute intervals throughout the three runs. By plotting the three sets of readings an average value of lapse rate was obtained and this was scaled to give the average lapse rate over a height band of 1000 ft.

For flights made on and after 31st May 1960 the same three runs were carried out but arrangements were made for the bridge output to be recorded continuously on a Beaudouin A.13 recorder. The lapse rate was obtained by analysing the record in a similar manner, except that the temperature readings were taken at shorter time intervals.

<u>í</u>	1	T T	1		1	1			M	ean valu	es of:]	
		ł	Maam	Uni abt	Snood	W	ind	1			T	Cloud			Distance	Number of
Flight	Date	Route	mean	Foot	Note V			Lapse	Viaihiliter	Screen	Dew	Cover (eights) - Type	- Base (1	000's ft)	Miles	5 ft/sec
NOo			CME	reet	MICUS	Speed	Direction	Rate	AISTOTTICA	Temp.	Point		1 34 7 1	TT-1 la	millob	Gusts/mile
			GRAIT			Knots	Degrees	°C/1000 ft	N. Miles	0°C	0°C	Low	Medium	High	and the second	-
	30/0/50		4 5 4 5	200	300	12	120	2.0	12	23	0	Nil	Nil	Nil	145.1	3.02
	2/10/50	2	1030	200	1 100	8	180	3.1	8	22	15	1 Cu 2°5	Nil	4 Ci 25	190-9	5.22
10	2/10/59	S	1500			10	200	1.5	9	22	14	1 Cu 4	3 Ac 14	1 Ci 20	105.5	4.46
11	5/10/59	E	1115		n	15	100	2.5	2	21	12	Nil	Nil	Nil	134.05	6.07
12	5/10/59	E	1500	n	11	15	100	3.0	3	20-	9 -	-Nil	Nil	Nil	172.0	3.95
13	7/10/59	s	1130	11	400	8	140	2.0	4	22	13	2 Cu 4	Nil	Nil	184.06	5°65
14	7/10/59	E	1530	er	. 11	3	100	0.5	5	22	11	Nil	Nil	Nil	101 • 3	0°11
17	14/10/59	S	1530	- 11	300	6	180	2.5	8	- 19	8	1 So 5	Nil	Nil	186.2	1.39
18	15/10/59	W	1515	88	11	5	120	2.5	11	16	9	2 Cu 3	Nil	Nil	96•2	2.84
19	16/10/59	S	1500	11	11	15	140	2.0	5	19	11	1 Cu 3°5	Nil	Nil	161.0	6°06
20	19/10/59	W	1145	11	1 11	18	320	3∘0	9	11	7	3 Cu 2 - 5 Sc 3	Nil	NIL	105.4	
21	22/10/59	S	1200	17	11	12	290	3°1	22	15	6	3 Cu 3	Nil	Nil	185.0	/°/5
23	23/10/59	E	1200	tt .	400	14	230	2.5	6	12	8	6 Sc 6	8 A0 15	NIL	194*1	
24	28/10/59	S	1515	19	300	12	300	3.8	4	9	3	$3 \text{ Cu } 2^{\circ}5 - 4 \text{ Cu } 5$	5 AC 10	NIL	190-4	5.82
25	5/11/59	S	1245			8	300	2.5	3	10	6	1 3 Cu 2°5 ~ 5 Sc 4°5			185.7	0.62
37	4/12/59	9	1600			18	300	2.5	15	6	2			1 7 US 22	187.8	9.21
38	8/12/59	S	1100			11	160	2.5		9	D E		NAJ		141.6	4.36
39	8/12/59	E	1600			19.2	125	1.9	4	10	2		NII	6 Ci 25	136.7	5.25
6/	31/5/60	L E	1515	11		46	090	2.0	5	19	15	12 St 1 = 1 Cu 2 = 6 Sc 1	Nil	Nil Nil	176.9	11.99
71	9/6/60	D C	4520	1 11	11	10	290	2.5	22	18		$3 \text{ Cu} 3^{\circ}2 = 4 \text{ Su} 5$	Nil	Nil	302.9	6.46
72	34/6/60	2	1100	n	н	11	260	3.1	22	17	11	4 Cu 2.5	Nil	Nil	178.6	9.16
81	8/7/60	S	1500	n	n	8	300	3.0	10	17	13	2 Cu 2 - 4 So 4	7 Ac 10	Nil	180.7	3.08
82	12/7/60	E	1145	11	n	16	260	2.5	14	19	11	3 Cu 3 - 4 So 5	3 Ac 12	Nil	168•2	6°92
91	29/7/60	W	1415			10	270	2.8	10	14	12	3 Cu 2°5 - 5 Sc 4	Nil	Nil	155.7	6•22
98	20/9/60	W	1045	11	11	12	340	~	10	11	6	2 Cu 2.5 - 5 Sc 4	Nil	Nil	129.3	9.47
100	23/9/60	W	1115	11	ų	7	360	3.4	11	13	9	3 Cu 2°5	Nil	5 Cs 20	135•8	3°43
102	5/10/60	S	1430	11	11	11	200	3°1	13	16	13	4 Cu 2	Nil	Nil	187.0	6.90
103	6/10/60	S	1115	11	11	8	140	2.5	9	16	13	7 Cu 2	Nil	Nil	170.1	6°16
107	12/10/60	W	1545	11	1	10	340	3.1	11	9	2	3 Cu 2.5	Nil	Nil	12/0/	5°92
111	28/11/60	S	1545			6	240	2.2	15	5	0	2 St 1°5	NIL	NIL	185'3	2-14
119	31/1/61	W	1145		11	10	200	3.5	8	5	3	4 Sc 2.5	8 AC 10	NIL	496.2	46.00
122	6/2/61	S	1530		250	24	260	3.8	38	8	1			N11 N57	100-2	10 99
124	9/2/61	E	1315		300	22	295	4°2	22	10) (), Ci 20	181.6	上。上1
128	6/3/61	W	1145			5	090	3.1	12	16	6		Nil	5 Ci 25	117-9	5.20
150	18/4/61	E	1500			0	155	3.2	22	10	z v	6 Cu /	Nil	Nil Nil	234.0	12.18
157	10/5/01	L D	1515			2) 8	200	2.5	8	12			Nil	Nil	171.6	5.56
140	15/5/61	2	11.1.5		,,	15	080	2.5	15	15	6	5 Sc 2.5	Nil	Nil	249.4	9.99
142	6/6/61	S	1500	11		2	350	2.8		22	13	1 Cb 2.8 - 5 Cu 3	Nil	Nil	186.4	3-62
145	13/6/61	E	1215			17.5	355	3.4	18	15	7	3 Cu 2.5 - 5 Sc 3	Nil	Nil	185•4	5.05
146	14/6/61	Ŵ	1445	n		7	140	3.5	11	18	9	2 Cu 2.5 - 6 Sc 4	Nil	Nil	173.8	4°36
147	15/6/61	E	1145			12	230	2.8	7	20	10	2 Cu 4	Nil	5 Ci 25	222.5	7°14
163	30/8/61	W	1400	l n	11	7	320	1.8	12	19	10	4 Cu 3	Nil	Nil	143.9	4.94
176	11/1/62	S	1500	n	11	30	270	2.8	16	8	1	5 Cu 2·5	Nil	3 Ci 25	297•8	14.73
178	12/1/62	S	1630	н	1 11	24	220	2.0	2	0	-2	Nil	Nil	1 Ci 25	149•8	8.99
181	7/2/62	S	1200	11	"	24	230	2.5	8	9	5	5 Cu 2	Nil	Nil	192.9	13.19
182	13/2/62	S	1200	17	11	20	320	3.0	22	5	-4	3 Cu 2	4 Ac 15	Nil	186.9	12.42
	ł				1			1	ł						L	

			Maan				Mean values	of :-			N	umbei	of	Gus	sts							Gust	s/Mil	e				Gust
Flight	Date	Route	Time	Height	Speed		Vind	Lapse	Distance			ł	rt/S	ec	-							ታዊ	/500	1				RMS
110.			GMT	TCCU	1110 03	Speed Knots	Direction Degrees	°C/1000 ft	MIICS	5	7.5	10	15	20	25	30	35	40	5	7.5	10	15	20	25	30	35	40	Ft/Seo
7	30/9/59	E	1515	200	300	12	120	2.9	145.1	438	95	22	1						3.02	0.65	0.15	0.01	Ar an					1.533
10	2/10/59	S	1500	11	Ħ	10	200	1.5	105.5	471	159	42	2						4.46	1.51	0.40	0.02						3.032
11	5/10/59	E	-111-5	tt,	<u> </u>	- 15	100	2.5	134.5		326	-103	6	1					<u> </u>	2.42	0.77	0.04	0.01					2.362
12	5/10/59 7/10/59	ь S	1130		400	8	140	2.0	184.6	1042	447	148	9						5.65	2.42	0.80	0.05						3.919
14	7/10/59	E	1530	11 14	tt 700	3	100	-0.5	101.3	11	1	1	1						0.11	0.01	0.01	0.01						0.317
17	14/10/59	5 ₩	1550		, 500 11	5	120	2.5	96.2	- 250 273	52 170	120	44	12	5	2			2.84	1.17	1.25	0.46	0.12	0.05	0.02			4.410
19	16/10/59	S	1500	11		15	140	2.0	161.0	976	415	147	9			。	-		6.06	2.58	0.91	0.06	0 52	0.21	0 08	0.03	0.01	3.533
20	19/10/59	₩ S	1145		tt tt	18	320 290	3.0 3.1	105.4	675 1434	668	289	43	22 7	22	1	2	1	7.75	4.47 3.61	1.56	0.23	0.04	0.02	0.01			3.511
23	23/10/59	Ē	1200	11	400	14	230	2.2	194.1	734	157	26	2				ł		3.78	0.81	0.13	0.01		0.07	0.01			2.120
24 25	28/10/59	S S	1515	11 11	300 "	12	300 300	3.8	190 . 4	21 <i>33</i> 328	1202	644	207 5	39	-6	ו			11.20 5.82	6.31 2.27	0.73	0.09	0.20	0.05	0.01			3.338
37	4/12/59	S	1600	rt	n	18	300	2.5	185.7	1786	849	370	42	5	2				9.62	4.57	1.99	0.23	0.03	0.01	-			3.604
38 70	8/12/59	S ភ	1100	11 11	1 11	11	160	2.5	187.8	1735	844	355	38	4	1				9.24	4.50	1.89	0.20	0.02	0.01				1.816
67	31/5/60	E	1515	n	n	8	090	2.8	136.7	718	272	78	8						5.25	1.99	0.57	0.06						3.553
71	9/6/60	S	1500		11 	16	230	3.1	176.9	2122	1358	910	286	80	31	8	2		11.99	7.68	5.14	1.62	0.45	0.18	0.05	0.01		4.924
72 73	10/6/60	S	1530			11	290	2•5 3•1	178.6	1635	865	407	68	9					9.16	4.84	2.28	0.38	0.05					4.299
81	8/7/60	S	1500	11		8	300	3.0	180.7	556	147	28	4						3.08	0.81	0.16	0.02	0.01					2.717
82	12/7/60	E	1145	π		16	260 270	2.5	168.2	1162 969	468 629	431	133	39	5				6.22	4.04	2.77	0.85	0.25	0.03				4.903
98	20/9/60	W	1045	n	n	12	340	-	129.3	1225	872	629	257	83	25	5			9.47	6.74	4.86	1.99	0.64	0.19	0.04			6.250
100	23/9/60	W	1115	et 11	11 11	7	360 200	3.4	135.8	465 1291	229 573	131	42	23	6	1			3. 43	1.69	1.10	0.16	0.17	0.04	0.01			3.919
102	5/10/60 6/10/60 -	S -	14.50	11	11	8	140	-2-5-	-170.1	-1048	-387	116	. 8	2					6.16	2.27	0.68	0.05	0.01					3.175
107	12/10/60	W	1545		u	10	340	3.1	127.7	500	331	215	78	29	5	1			3.92	2.59	1.68	0.61	0.23	0.04	0.01			2.830
111	28/11/60	S W	1545			10	240	2.2	66.7	297 473	263	147	42	13	2	1			7.09	3.94	2.20	0.63	0.19	0.03	0.02			4.167
122	6/2/61	S	1530		250	24	260	3.8	186.2	3165	1987	1172	313	77	21	7	2	1	16.99	10.67	6.29	1.68	0.41	0.11	0.04	0.01	0.01	5.299
124	9/2/61	E	1315		300	22	295	4.2	132.5	1382	615 ム33	250	58 38	8 5	1				4.41	2.38	1.22	0.29	0.03	0.01				4.118
130	18/4/61	Ē	1500	Π	n	8	135	3.1	117.9	613	211	52	4						5.20	1.79	0.44	0.03						3.450
137	8/5/61	E	1515	11	n	25	280	3.2	234.0	2849	1533	105	136	22	3				12,18	6.55	0.61	0.58	0.09	10.01	ļ			3.408
140	15/5/61	S	1500	n		15	035	2.5	249.4	2491	1122	455	62	14	1				9.99	4.05	1.82	0.25	0.06		ł			3.492
144	6/6/61	S	1500		π	2	350	2.8	186.4	674	237	81	8						3.62	1.27	0.43	0.04						2.459
145 146	13/6/61	Ew	1215	н 1	т т	17.5	355 140	2•4 3•5	185.4	920 758	004 418	234	ر 48	10	3				4.36	2.40	1.35	0.28	0.06	0.02				3.939
147	15/6/61	E	1145	n	n	12	230	2.8	222.5	1589	648	211	16	2					7.14	2.91	0.95	0.07	0.01	0.07	0.01			3.577
163 176	30/8/61	W	1400	11 11	11 11	7	320 270	1.8	143.9 297 8	710 ⊥387	4 39 2791	1712	1477 1772	18	4 17	2			4•94 14•73	9.37	5.75	1.49	0.33	0.06	0.01	1		5.171
178	12/1/62	S	1630	Ħ	=	24	220	2.0	149.8	1346	638	258	32	3					8.99	4.26	1.72	0.21	0.02				1	3.921
181	7/2/62	S	1200	11 11	n	24	2 3 0	2.5	192.9	2535 2301	1514	826	169 61	24	5				13.19	7.85 8.10	4.27 5.00	1.33	0.12	0.02	0.01			5.446
102	1 2/ 02	6	1200			20	J20	J.U	100.7	- 724														<u> </u>			1	

Flight	Date	Route	Number of times each gust speed was exceeded. Distance Miles Number of times each gust speed was exceeded.																		
110.				-40	-35	-30	- 25	-20	- 15	-10	. 7•5	 5	5	7.5	10	15	20	25	30	35	40
7 9 10 11 12 13 14 17 18 19 20 123 24 25 37 8 39 67 17 27 31 82 91 80 102 103 107 119 122 4 128 130 142 144 51 46 147 167 178 181 182	30/9/59 2/10/59 2/10/59 5/10/59 5/10/59 7/10/59 7/10/59 14/10/59 15/10/59 15/10/59 15/10/59 22/10/59 23/10/59 23/10/59 23/10/59 23/10/59 23/10/59 31/2/59 8/12/59 8/12/59 8/12/59 8/12/59 8/12/59 8/12/59 8/12/59 8/12/59 8/12/59 31/5/60 10/6/60 12/7/60 29/7/60 23/9/60 23/9/60 5/10/60 6/10/60 12/10/60 23/9/60 5/10/60 6/10/60 12/10/60 31/1/61 6/2/61 15/5/61 15/5/61 15/5/61 15/5/61 15/5/61 15/5/61 15/5/61 15/6/61 15/6/61 15/6/61 15/6/61 15/6/61 15/6/61 15/6/61 15/6/61 15/6/61 15/6/61 15/6/61 12/1/62 7/2/62 13/2/52	ESSEESESWSWSFSSSSEESSSSEWWWSSSWSEWEESSSEWEWSSSSSSSS	145.1 190.9 105.5 134.5 172.0 184.6 101.3 186.2 96.2 161.0 105.4 185.0 194.1 190.4 56.4 185.7 187.8 141.6 136.7 176.9 302.9 178.6 180.7 168.2 155.7 129.3 135.8 187.0 170.1 127.7 185.3 66.7 186.2 132.5 181.6 117.9 234.0 171.6 249.4 185.4 185.4 185.4 185.4 185.4 185.4 185.4 185.4 185.4 185.2 143.9 297.8 149.8 192.9 186.9	1	2	4 3 1 4	3 1 1 12 3 11 1 1 3 11 1 1 1 1 7 2 7	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 173 \\ 444 \\ 192 \\ 348 \\ 259 \\ 457 \\ 2 \\ 99 \\ 143 \\ 319 \\ 616 \\ 319 \\ 616 \\ 319 \\ 616 \\ 319 \\ 616 \\ 319 \\ 616 \\ 310 \\ 615 \\ 233 \\ 156 \\ 318 \\ 315 \\ 31$	$\begin{array}{c} 265\\ 5579\\ 4&28\\ 1&1\\ 5&36\\ 3&23\\ 4&39\\ 1&1\\ 5&36\\ 3&23\\ 1&1\\ 9&357\\ 1&9\\ 8&29\\ 6&21\\ 6&247\\ 6&247\\ 2&00\\ 3&26\\ 1&266\\ 1&266\\ 1&266\\ 1&266\\ 3&260\\ 2&299\\ 1&200\\ 1&268\\ 3&2190\\ 1&268\\ 3&2190\\ 1&280\\ $	$\begin{array}{c} 62\\ 241\\ 104\\ 198\\ 153\\ 278\\ 1\\ 32\\ 97\\ 246\\ 256\\ 396\\ 106\\ 728\\ 83\\ 497\\ 104\\ 134\\ 694\\ 468\\ 74\\ 264\\ 354\\ 102\\ 83\\ 102\\ 821\\ 179\\ 569\\ 127\\ 163\\ 366\\ 230\\ 14035\\ 775\\ 765\end{array}$	$\begin{array}{c} 14\\ 83\\ 31\\ 64\\ 52\\ 97\\ 1\\ 6\\ 791\\ 96\\ 791\\ 96\\ 791\\ 922\\ 214\\ 34\\ 227\\ 214\\ 34\\ 227\\ 214\\ 34\\ 227\\ 214\\ 34\\ 227\\ 214\\ 34\\ 79\\ 247\\ 367\\ 97\\ 140\\ 8617\\ 357\\ 177\\ 454\\ 223\\ 519\\ 14,5\\ 350\\ 197\\ 440\\ 470\\ 470\\ 470\\ 470\\ 470\\ 470\\ 47$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$5 \\ 19 \\ 3 \\ 5 \\ 1 \\ 19 \\ 2 \\ 14 \\ 5 \\ 2 \\ 2 \\ 10 \\ 1 \\ 2 \\ 3 \\ 4 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 $	2 8 1 1 2 1 3 2 1	3	1

TABLE 4. Sussex - effect of wind speed on turbulence

Range of Wind	Mean Wind in Range	Miles	5 Ft/Sec	5 Ft/Sec
Knots	Knots		Gusts	Gusts/Mile
Lapse Rate Range	e 2.0 - 2.4 ⁰ C/1000 ft			
6 - 10	7	369 . 9	1439	3.92
11 - 15	15	161	976	6.06
21 - 25	24	149.8	1346	8.99
Lapse Rate Range	e 2.5 - 2.9 ⁰ C/1000 ft			
0 - 5	2	186.4	674	3.62
6 - 10	7.8	887.2	4547	5.11
11 - 15	12.3	615.8	5861	9.52
16 - 20	18	185.7	1786	9.62
21 - 25	24	192.9	2335	13.19
26 - 30	30	297.8	4387	14.73
Lapse Rate Range	≥ 3.0 - 3.4°C/1000 ft			
6 - 10	8	371.6	1553	4.18
11 - 15	11.3	550.6	4360	7.92
16 - 20	18	363.8	4446	12.23
Lapse Rate Range	≥ 3.5 - 3.9°C/1000 ft			
11 15	12	190.4	2133	11.20
21 25	24	186.2	3165	16.99

TABLE 5. Sussex - effect of lapse rate on turbulence

Range of Lapse Rate °C/1000 ft	Mean Lapse Rate in Range ^O C/1000 ft	Miles	5 Ft/Sec Gusts	Gusts/Mile		
Wind Range 5 - 8 Knot	ĴS					
2.0 - 2.4 2.5 - 2.8 2.9 - 3.2	2.1 2.5 3.05	369 .9 584 . 3 371.6	1439 2589 1553	3.89 4.43 4.18		
Wind Range 9 - 12 Kno	ots					
1.5 - 2.0 2.1 - 2.5 3.1 - 3.5 3.6 - 4.0	1,5 2.5 3.1 3.8	105.5 490.7 550.6 190.4	471 3693 4360 2133	4.46 7.53 7.92 11.20		
Wind Range 21 - 24 Kr	nots					
2.0 - 2.4 2.5 - 2.9 3.5 - 3.9	2.0 2.5 3.8	149.8 192.9 186.2	1346 2535 3165	8.99 13.19 16.99		



SCALE I"= 60 MILES.

FIG. I. MAP OF LOW LEVEL ROUTES AND METEOROLOGICAL STATIONS.







FIG. 2. CONTOUR OF GROUND ALONG THE ROUTES.



FIG. 3. GUST SPECTRA FOR THE THREE ROUTES-ALL FLIGHTS.



FIG. 4. SUSSEX-EFFECT OF WIND SPEED ON TURBULENCE.



FIG. 5. SUSSEX-EFFECT OF WIND SPEED ON TURBULENCE FOR FOUR RANGES OF LAPSE RATE (GROUPED DATA)



FIG. 6. SUSSEX-EFFECT OF LAPSE RATE ON TURBULENCE







FIG. 8. EAST ANGLIA-EFFECT OF WIND SPEED ON TURBULENCE.



FIG. 9. EAST ANGLIA-EFFECT OF LAPSE RATE ON TURBULENCE.



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FIG. IO. WALES-EFFECT OF WIND SPEED ON TURBULENCE.



FIG. II. WALES-EFFECT OF LAPSE RATE ON TURBULENCE.



FIG. 12. COMPARISON BETWEEN THE SUSSEX AND EAST ANGLIAN ROUTES FOR FLIGHTS MADE IN SIMILAR METEOROLOGICAL CONDITIONS.



FIG. 13. COMPARISON BETWEEN GUST SPECTRA OBTAINED IN U.K. AND NORTH AFRICA.

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